

The background of the slide features a large, semi-transparent seal of the University of Almería. The seal is circular, with a central sunburst or star-like emblem. Around the emblem, the Latin motto "IN LUMINE SAPIENTIAE" is written in an arc at the top, and "UNIVERSITAS ALMERIENSIS" is written in an arc at the bottom. The entire seal is rendered in a light blue color that blends with the blue gradient background.

Fotobiorreactores para la producción masiva de microalgas

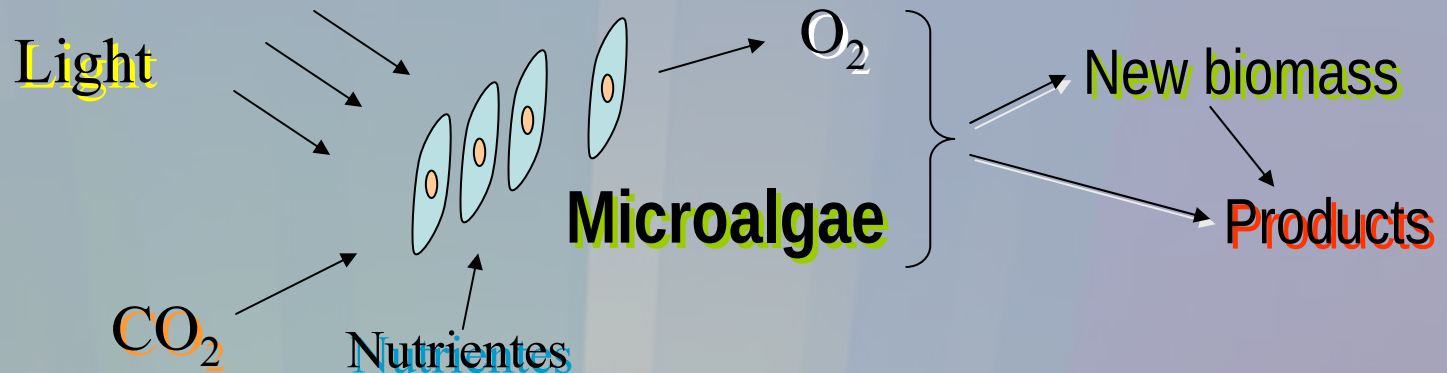
**Acien Fernández F.G.; García Camacho F.;
Fernández Sevilla J.M. y Molina Grima E.**

Objectives

- Reviewing the major types of photobioreactors used for the culture of microalgae.
- Principles of fluid mechanics, gas-liquid mass transfer and irradiance controlled microalgal growth will be integrated into a method for design bubble columns and tubular photobioreactors.
- Scale-up.

Photobioreactor design issues

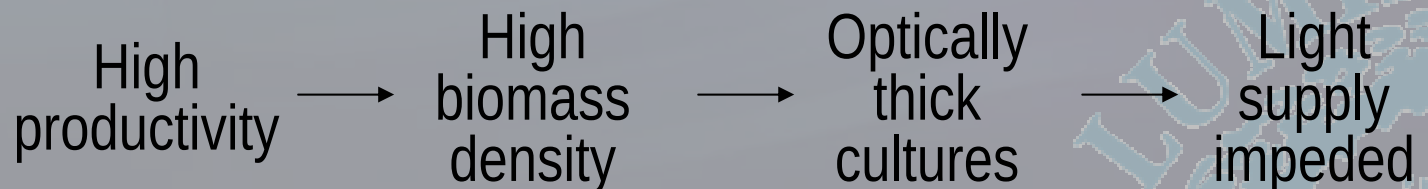
Light
limited
growth



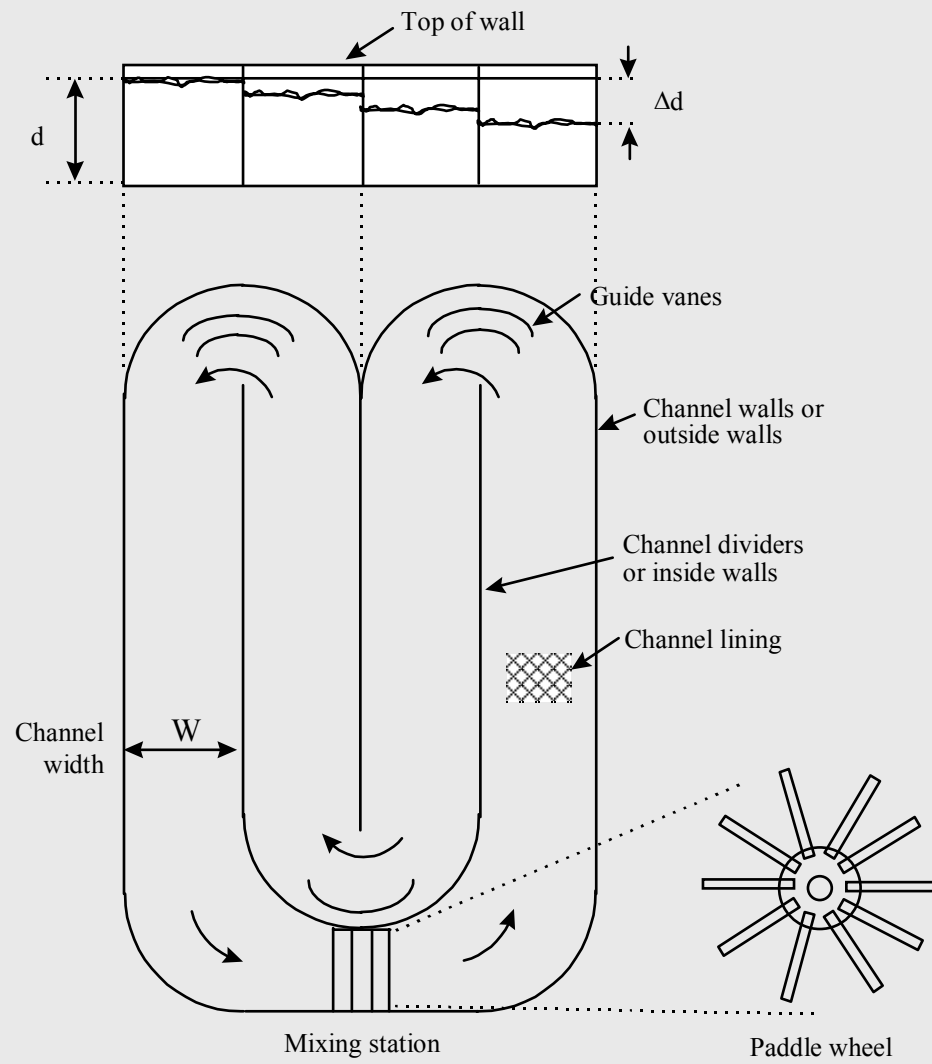
microalgal
culture
systems

- Supply sufficient light to support high growth rate (μ)
- Support high biomass density (C_b) for
 - High productivity (P_b)
 - Complete light harvesting
- Supply CO₂, remove O₂, mixing

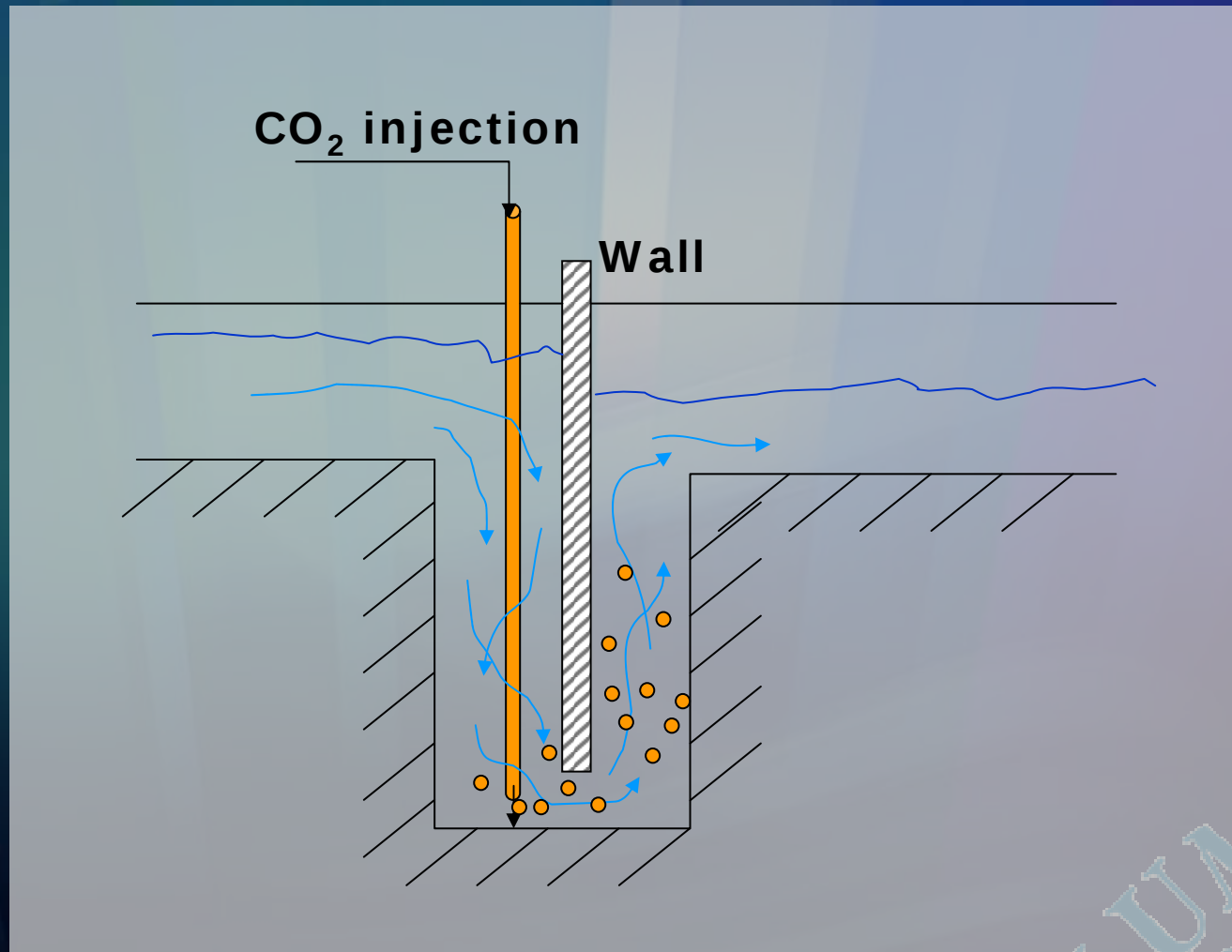
Light
limited
growth



Open raceways (1): description



Open raceways (2): CO₂ supply



Open raceways (3): mixing

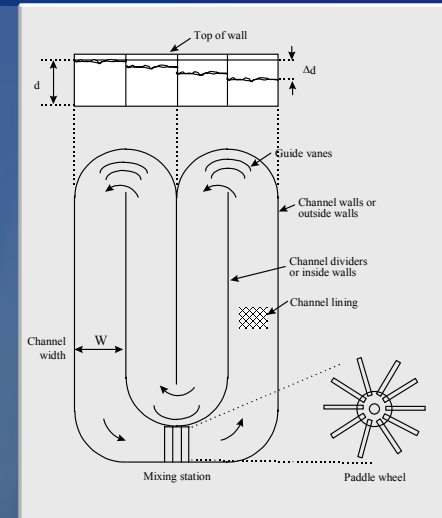
- Mean channel velocity, v (m s^{-1})

$$v = \frac{1}{n} R^{2/3} \cdot S^{1/2}$$

$n = 0.008 - 0.03$, manning friction factor

R = Hydraulic radius

S = Energy loss rate per unit length in the channel



- Channel length, L (m)

$$L = \frac{\Delta d (dw / (w + 2d))^{4/3}}{V^2 \cdot n^2}$$

- Paddle wheel's power requirements, P (kW)

$$P = \frac{Q \cdot \rho \cdot \Delta d}{\eta}$$

Open raceways (4): drawbacks

- Contamination and temperature are difficult to control
- The culture depth cannot be reduced below 12 to 15 cm or a severe reduction of flow and turbulence would occur
- Large areal volumes of 120-150 L m⁻² are usual and therefore low cell concentration is attained (≈ 500 mg L⁻¹)
- Low cell concentration increases the cost of harvesting

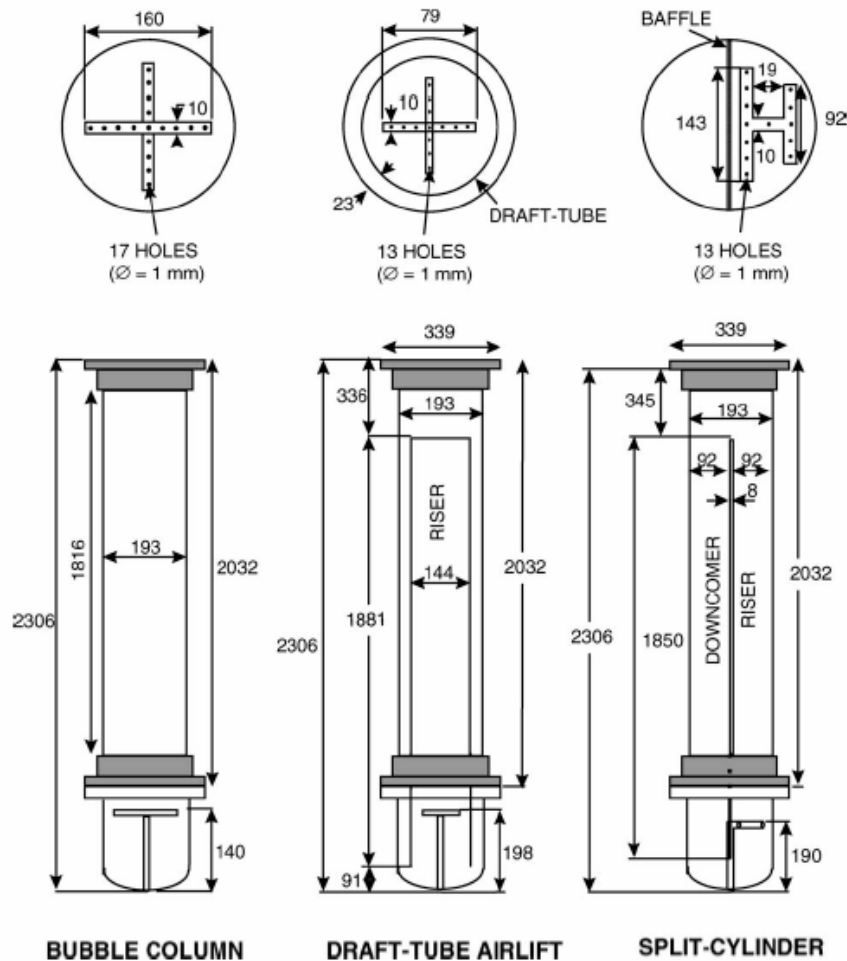
Enclosed photobioreactors

- Tubular

- Bubble column type
- Horizontal and fence configuration

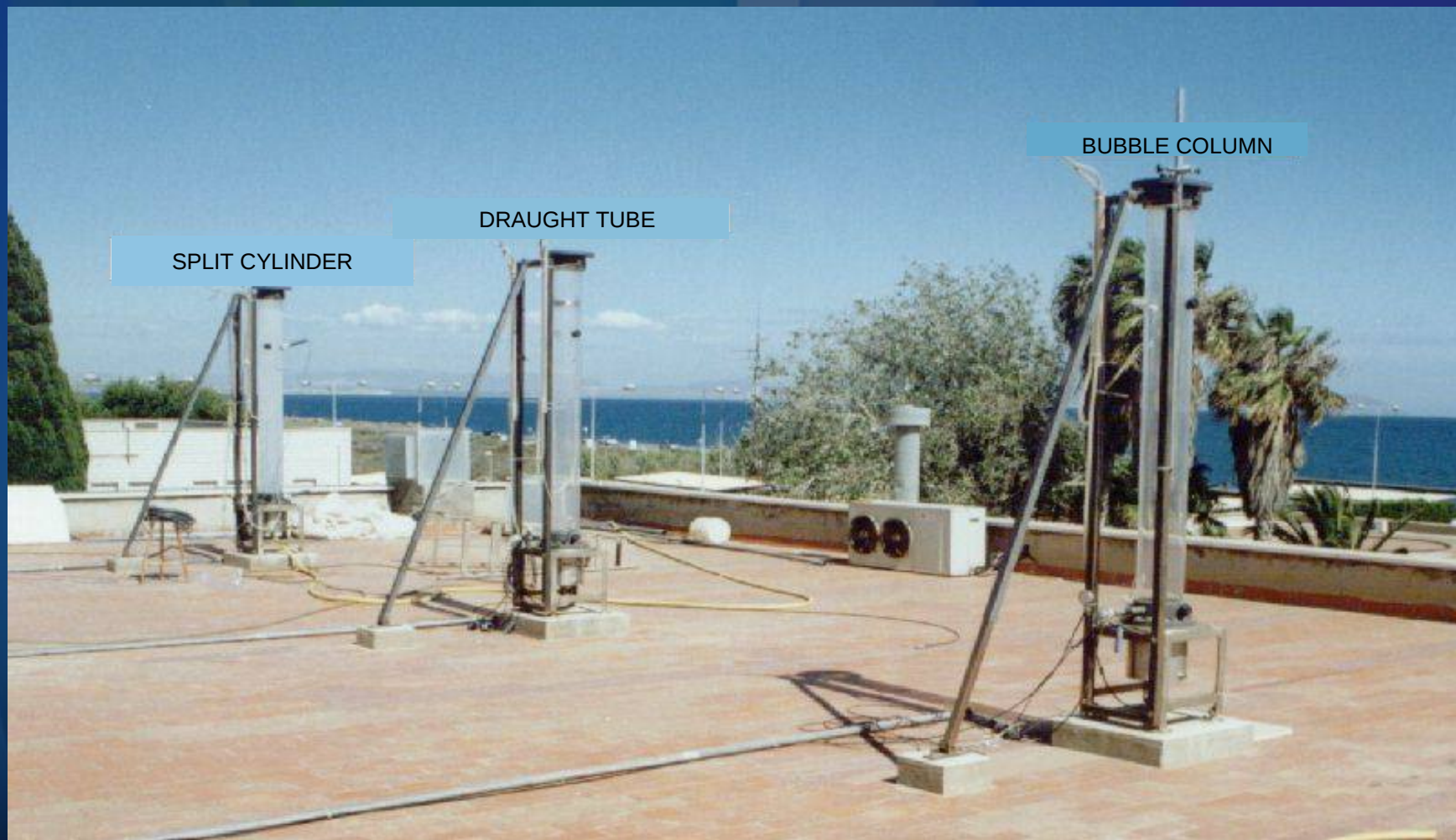
- Flat plate

Bubble column type photobioreactors (1)



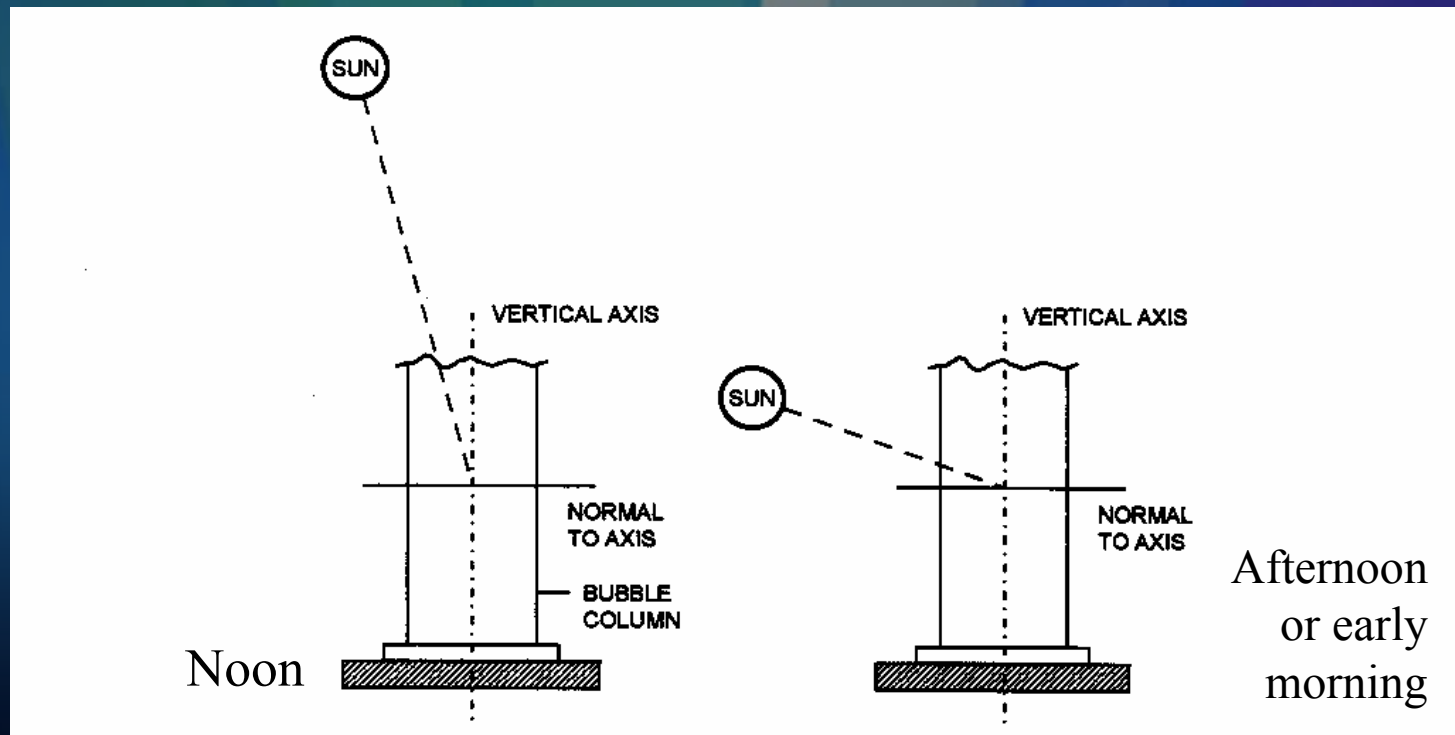
Sánchez Mirón et al., 2000 Aiche Journal, 46, 1872-1887

Bubble column type photobioreactors (2)



Bubble column type photobioreactors (3)

- Height of only a few meters
- Major advantage: oxygen does not accumulate
- Easy to keep sterile compared to other tubular systems
- Major drawback: the reactor is always at a large angle to the sun's rays



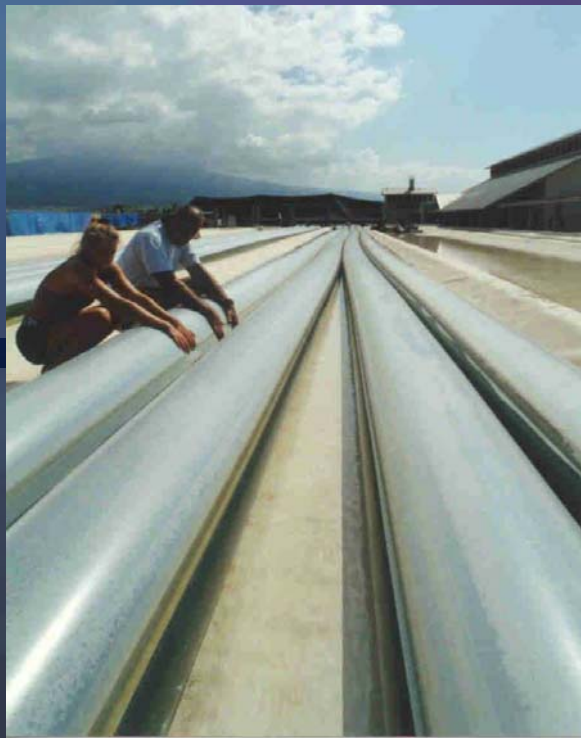
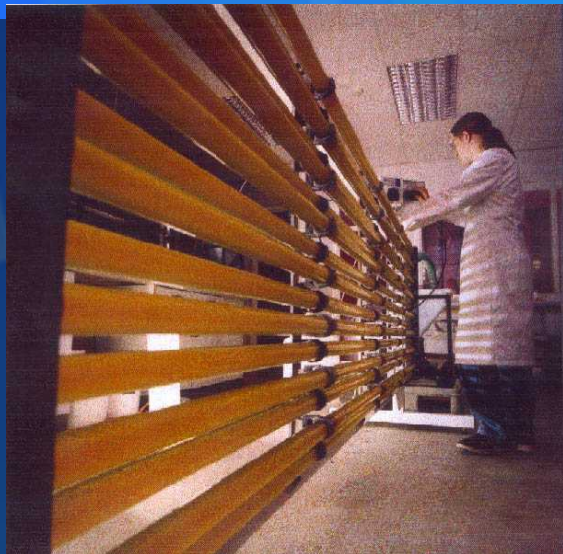
The amount of solar energy absorbed is lower than for horizontally placed reactor

Tubular photobioreactor (1)

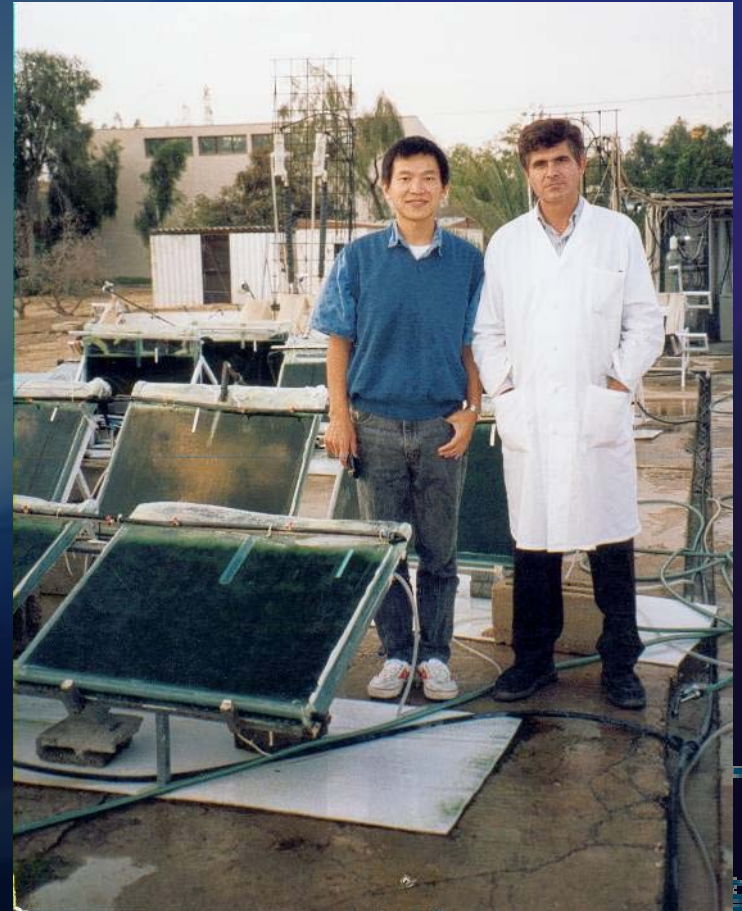
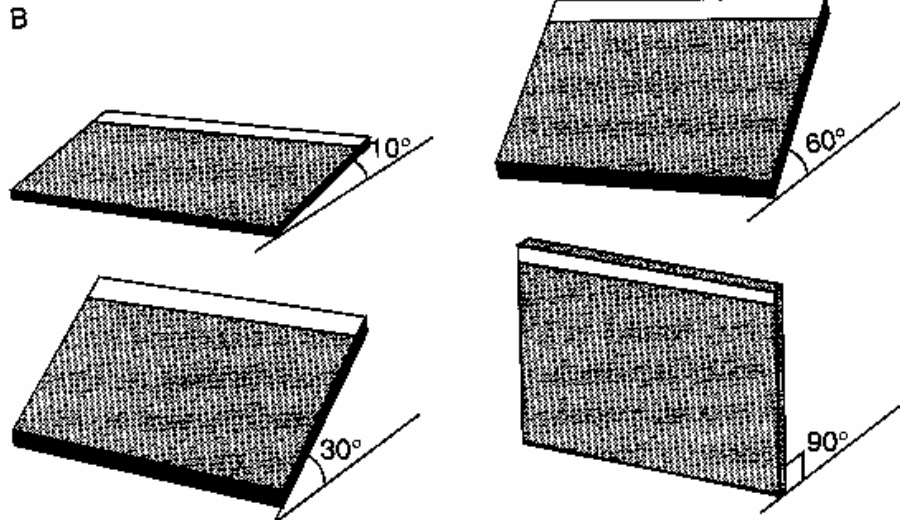
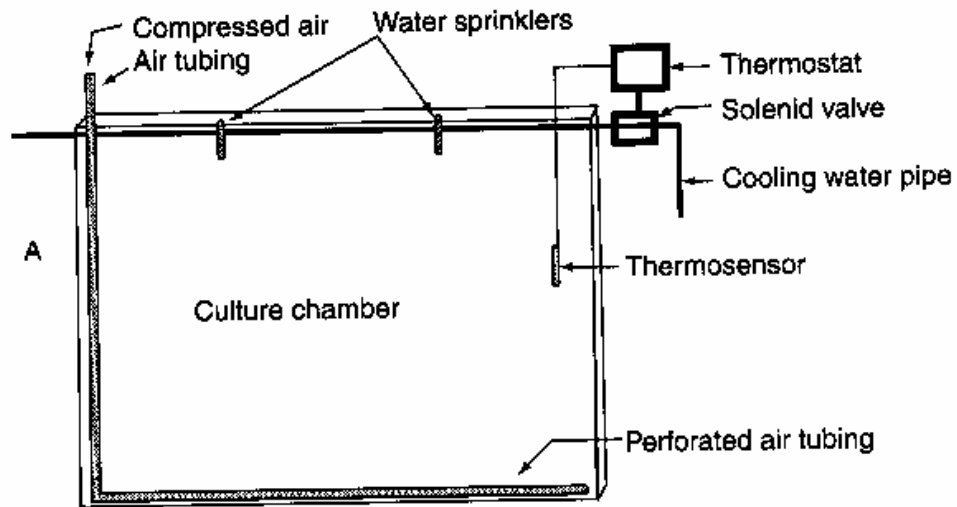
- Solar loop: arranged to optimally harvest sunlight.
- Solar loop: arranged to minimize land occupation
- Airlift system: adequate pumping and effective gas removal



Tubular photobioreactors (2)



Flat plate reactors (1)



Flat plate reactors (2)

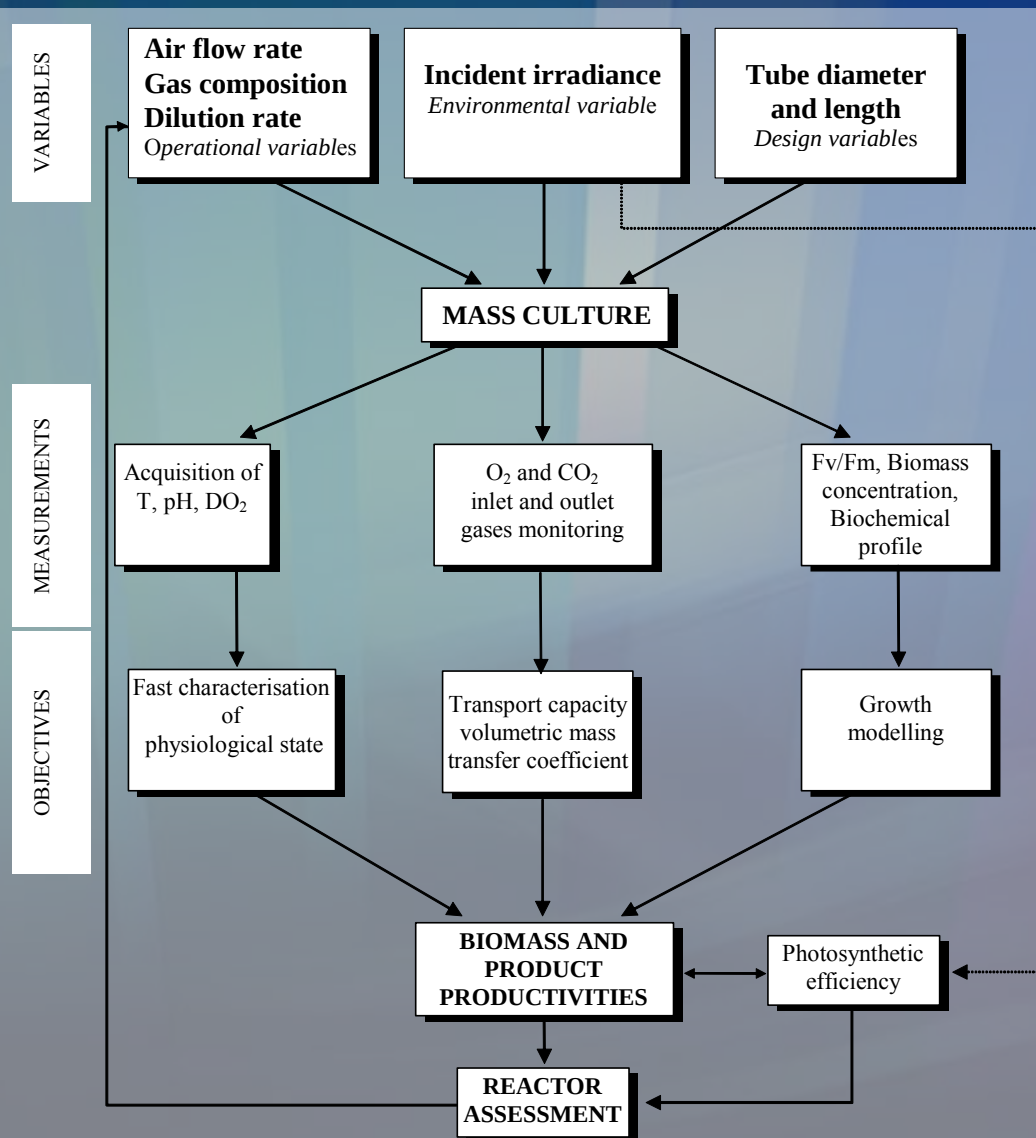


Flat plate reactors (3)

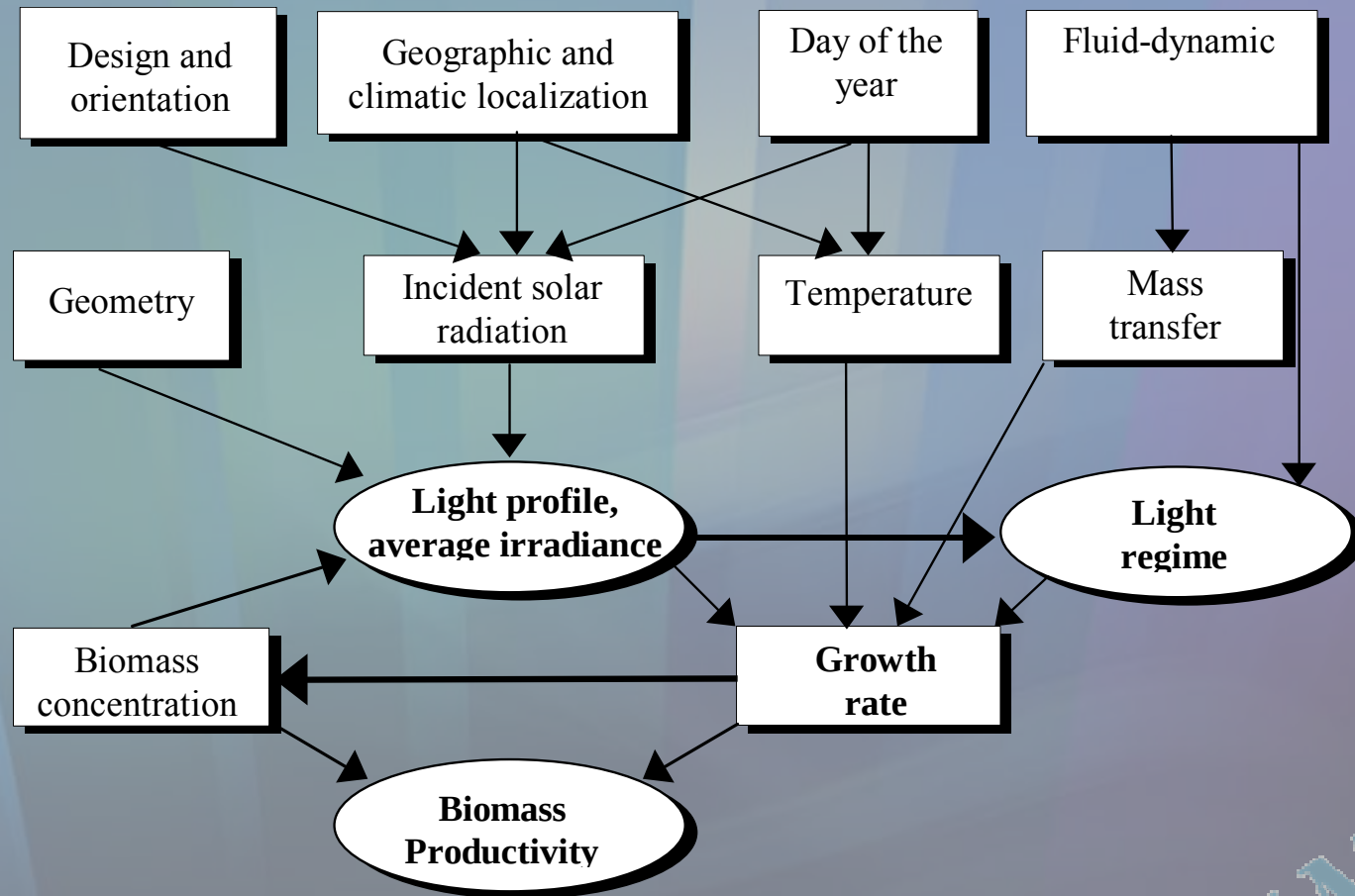


- Drawback**
- Difficulty in maintaining an adequate turbulence, buildup of O_2 (up to $30-40 \text{ mg L}^{-1}$); fouling
- Merit**
- Illuminated surface over 500 m^2 could be set up on a ground area of 100 m^2
 - Lamination of irradiance → enhancement of light efficiency

Main variables to be assessed and their impact on the reactor's performance



Relationship among parameters that influence biomass productivity



E. Molina Grima 1999, Encyclopedia of Bioprocess Technology: Fermentation, biocalysis and Bioseparations. 1753-1769, John Wiley and Sons Inc.

Design of tubular reactors



Design strategy (1)

Biomass productivity must be optimized.

$$Pb_v = \mu \cdot C_b$$

$g L^{-1} d^{-1}$

$$\mu = \frac{\mu_{\max} \cdot I_{av}^n}{I_k^n + I_{av}^n}$$

$$I_{av} = \frac{I_o}{\phi_{eq}} \left(1 - \exp(-\phi_{eq} \cdot K_a \cdot C_b) \right)$$

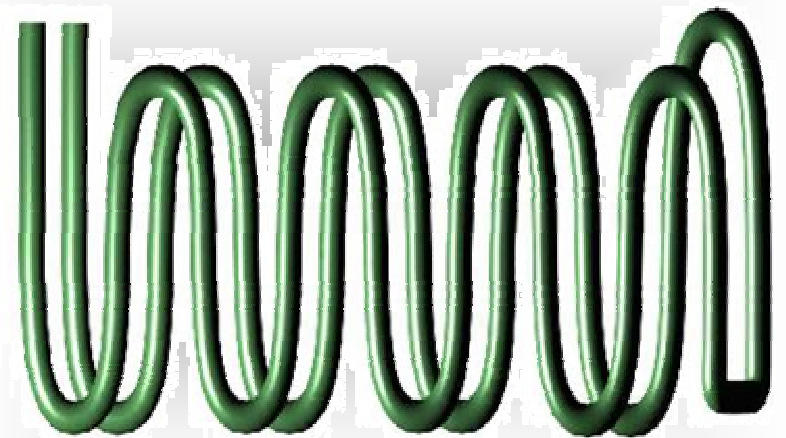
$$\phi_{eq} = \frac{d_t}{\cos(\theta)}$$

$$Pb_a = Pb_v \frac{\pi \cdot d_t}{4 \cdot n_T}$$

$g m^{-2} d^{-1}$

Design strategy (2)

- ✓ I_o must be maximized.
 - ✓ $I_o = f(\text{location, weather, geometric arrangement})$
- ✓ The arrangement of tubes controls the mutual shading.
- ✓ Maximizing land use



Design strategy (3)

- Liquid velocity

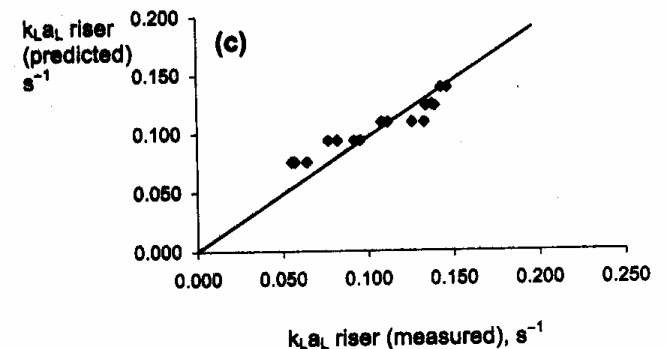
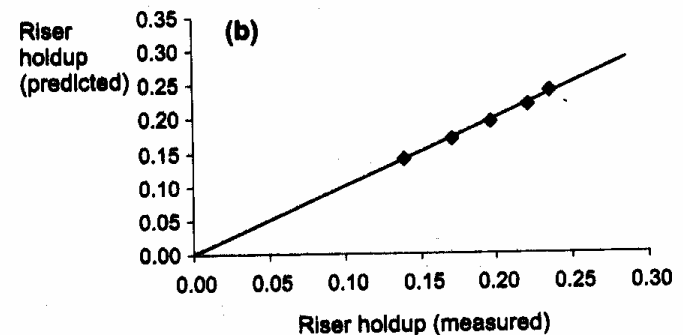
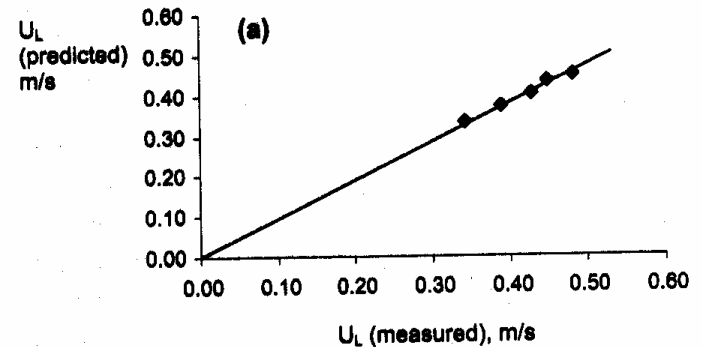
$$U_L = \left(\frac{g \cdot \varepsilon_r \cdot h_r \cdot d_t^{1.25}}{0.316 \cdot \left(\frac{\mu_L}{\rho} \right)^{0.25} \cdot L_{eq}} \right)^{4/7}$$

- Gas holdup

$$\varepsilon_r = \frac{\beta}{\lambda + \frac{u_b}{u_g + u_L}}$$

- $K_L a$

$$\frac{k_L}{d_b} = \frac{k_L \cdot a_L}{6 \cdot \varepsilon_r} (1 - \varepsilon_r)$$



Design strategy (4)

- ✓ The maximum continuous run length of the solar tube is limited by a combination of factors.

$$L = \frac{u_L ([O_2]_{in} - [O_2]_{out})}{RO_2}$$

Design strategy (5)

- The airlift system should satisfy the principal demands:
 - Effective circulation of the fluid
 - Effective separation of gas and liquid
- The airlift system should be small



Design strategy (5)



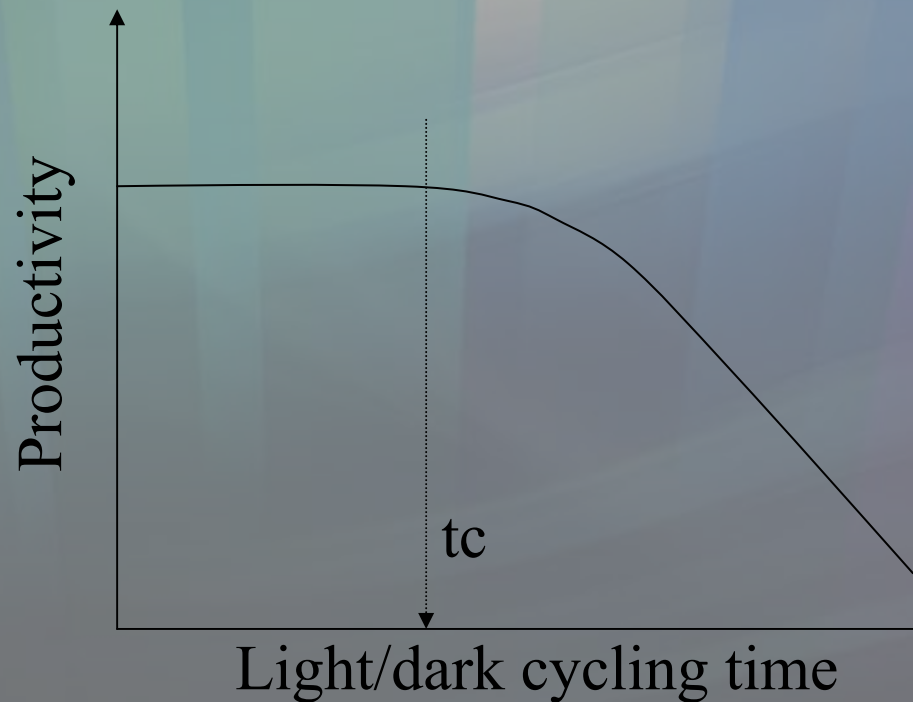
Scaleup approaches

$$V = \frac{\pi \cdot d_t^2}{4} \cdot L$$

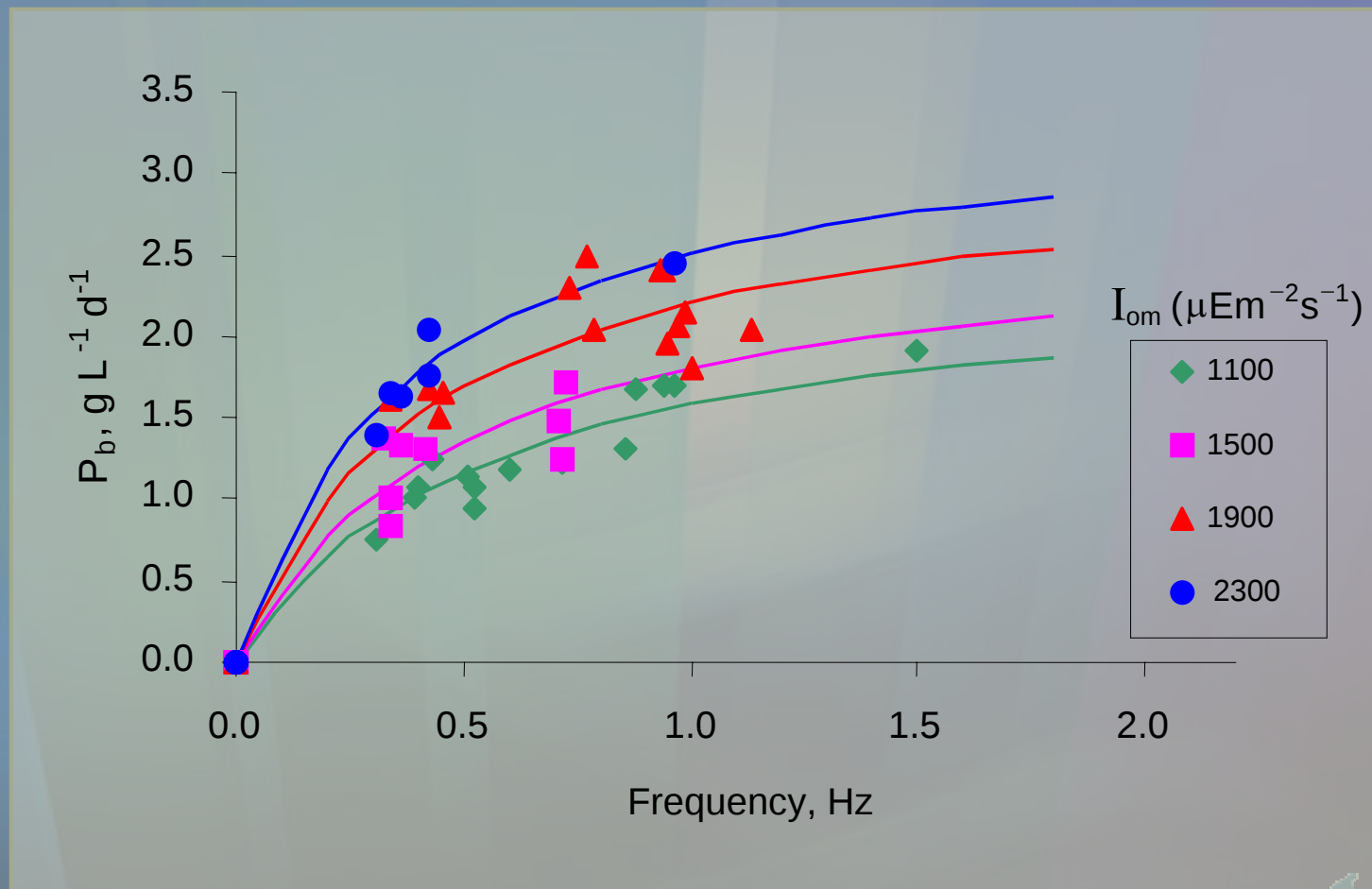
- The only variable that can be scaled up is d_t
- d_t determines the tube length
- Then, multiple modules of identical type

The scaleup criterion

- The frequency of the light/dark cycle interchange is held constant upon scale up.

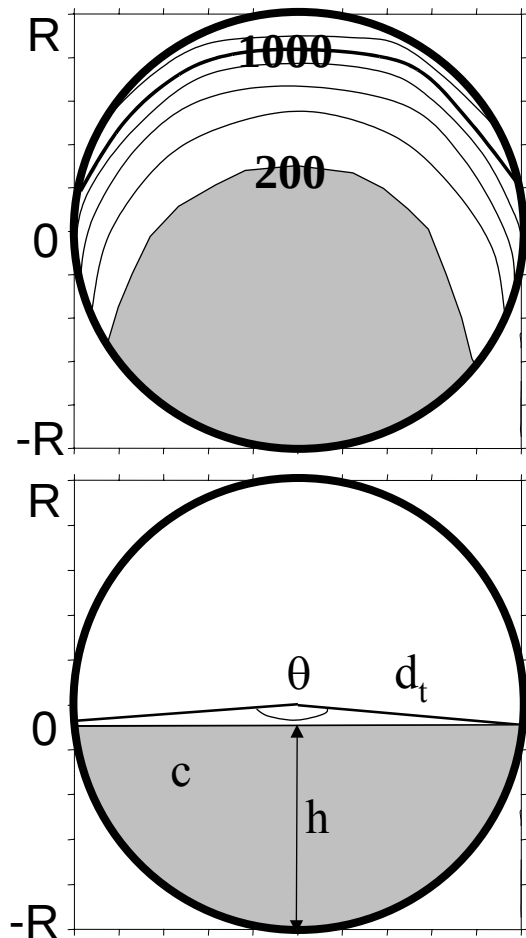


Scaleup considerations



E. Molina Grima et al. (2001) J. Biotechnol 92, 113-131

The scaleup criterion



$$Q_R = \frac{\text{Dark zone volume}}{t_d}$$

$$U_R = \frac{Q_R}{\text{Surface}}$$

$$\Phi = \frac{V_f}{V_f + V_d}$$

$$v = \frac{1 - \Phi}{t_d}$$

[http://www.ual.es/Universidad/Depar/IngQuimi/contenido/l\(r\).htm](http://www.ual.es/Universidad/Depar/IngQuimi/contenido/l(r).htm)

The scaleup criterion

$$\boxed{\frac{d_{tL} U_{RS}}{a d_{tS} U_{RL}} = 1} \Rightarrow U_{RL} = \frac{f}{a} U_{RS}$$

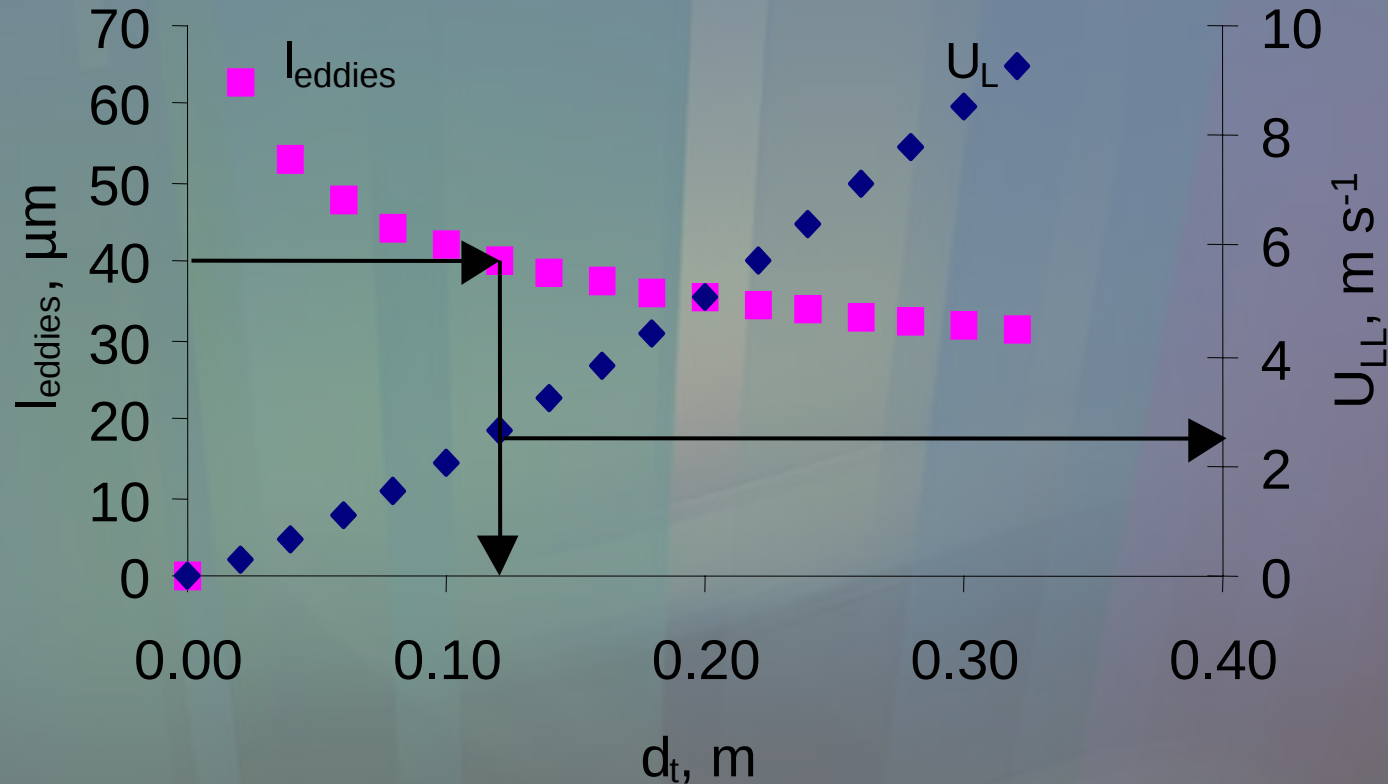
$$f = \text{scale factor} = \frac{d_{tL}}{d_{tS}}$$

$$a = \frac{1 - \Phi_L}{1 - \Phi_S}$$

$$U_R = 0.2 \frac{U_L^{7/8} v^{1/8}}{d_t^{1/8}}$$

$$U_{LL} = \frac{f^{9/7}}{a^{8/7}} U_{LS}$$

Maximum scaleable tube diameter



$$u_{ll} = \frac{f^{9/7}}{a^{8/7}} \cdot u_{ls}$$

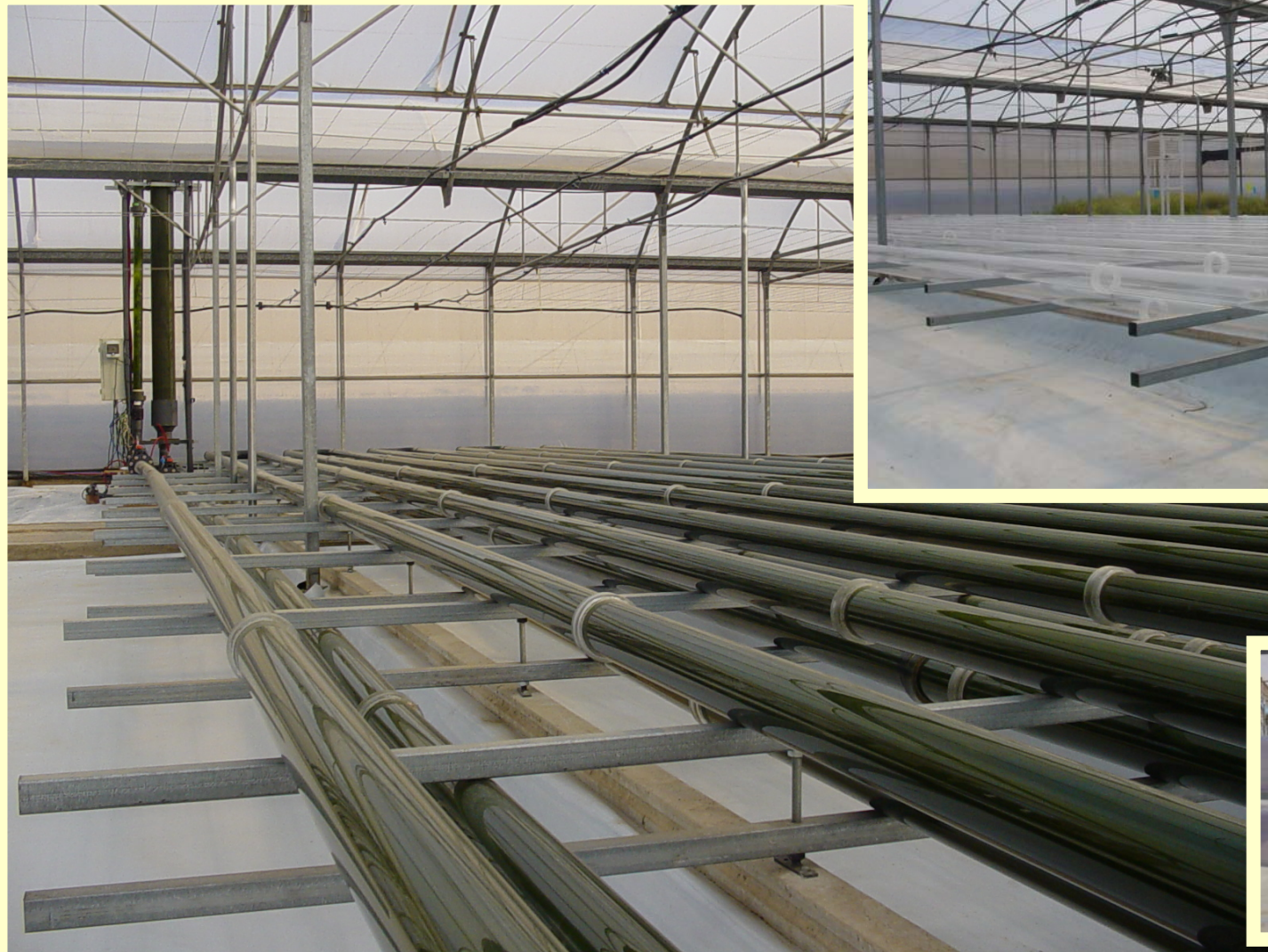
Contreras et. al (1998), Biotechnol. Bioeng. (60) 317-323

$$\left. \begin{array}{l} \lambda < 45 \mu\text{m} \\ \gamma > 7000 \text{ s}^{-1} \end{array} \right\}$$

Harmful to *P. Tricornutum* cells

C. Brindley Alias et al. (2004) Biotechnol Bioengng., in press.

The industrial-scale reactor and the microalgal production system



The industrial-scale reactor and the microalgal production system



Fotobiorreactor tubular industrial





Departamento de Ingeniería Química

Universidad de Almería